

# Tribological model system testing of cocoa mass samples with different particle size distributions

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## Background and motivation: Food processing, structure and mouthfeel

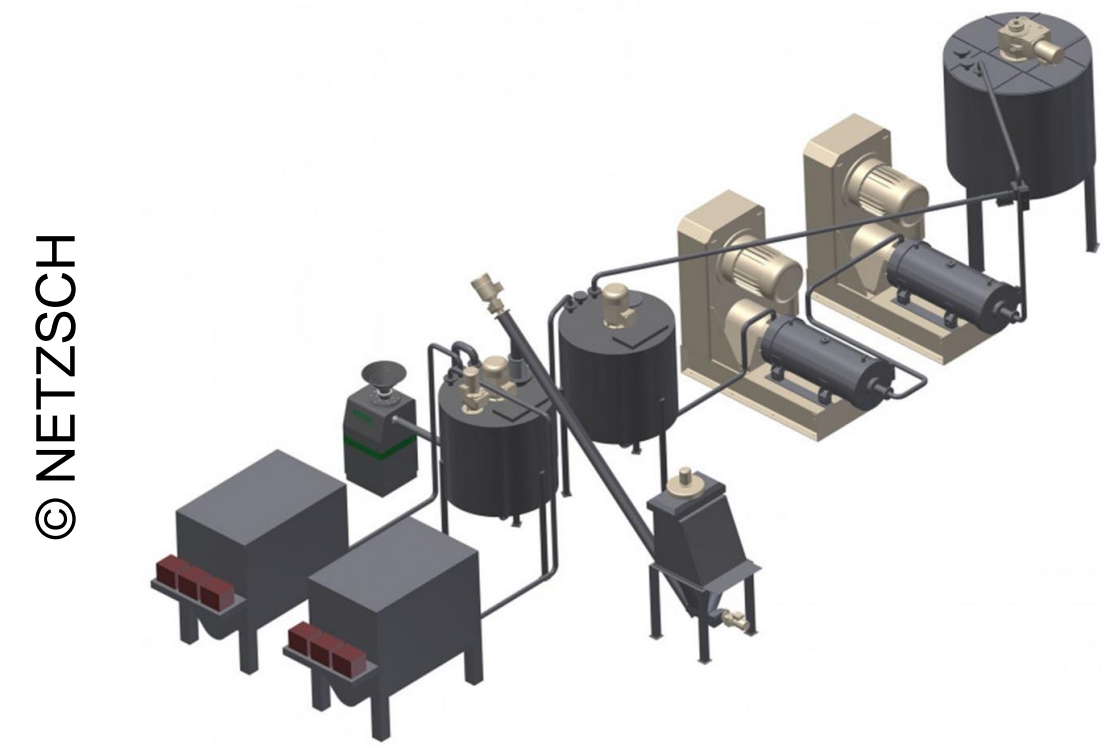


Fig. 1 Model of a confectionery mass production line

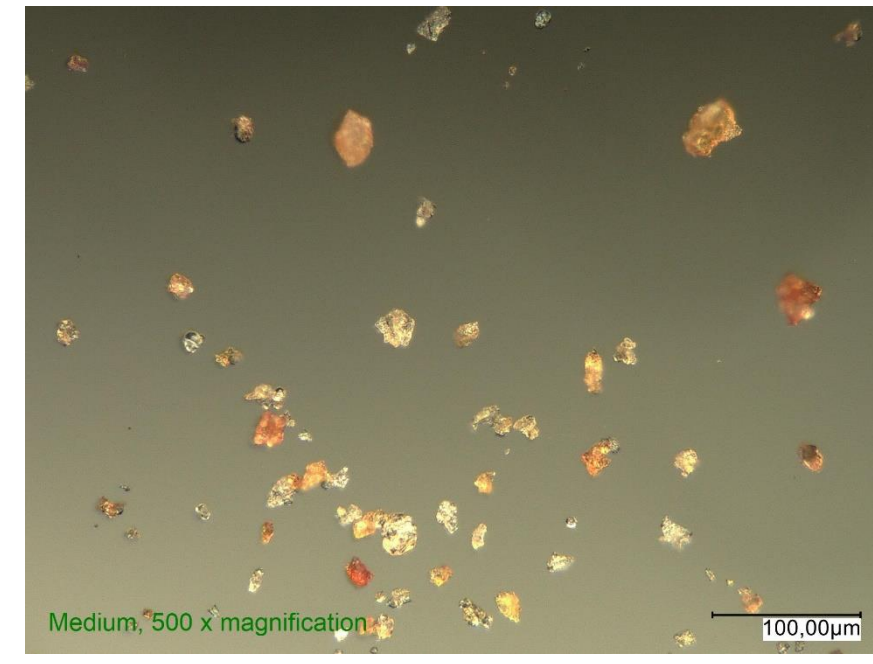


Fig. 2 Light microscopy image of cocoa mass particles

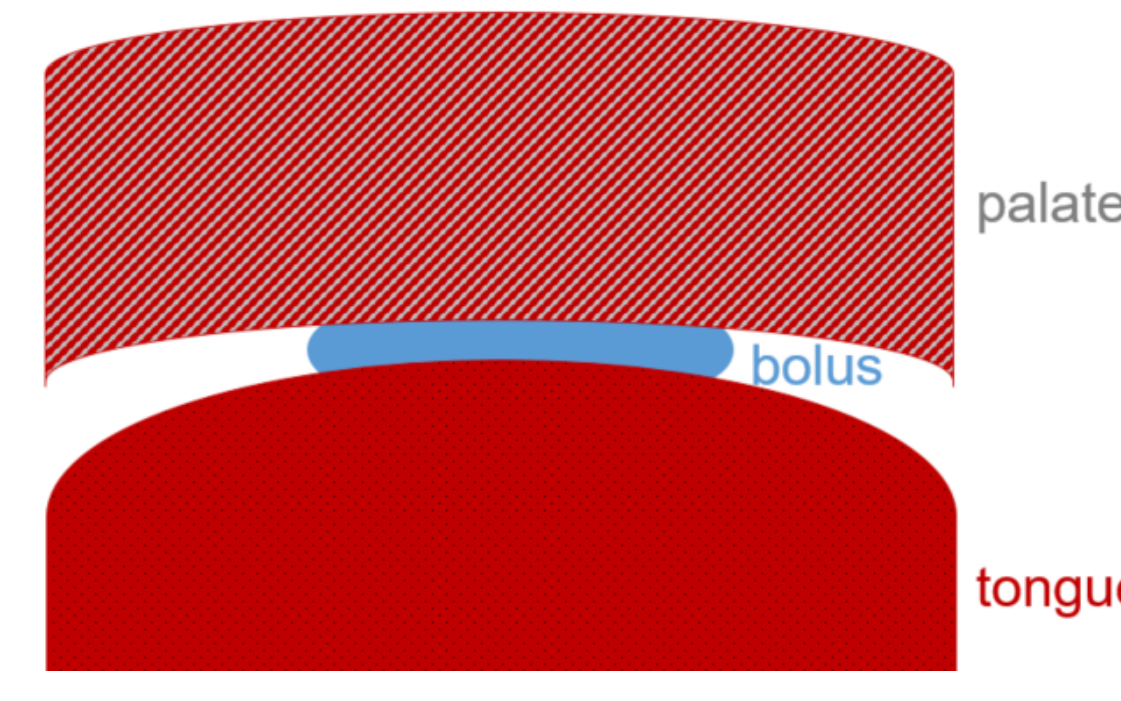


Fig. 3 Real-world tribosystem schematic

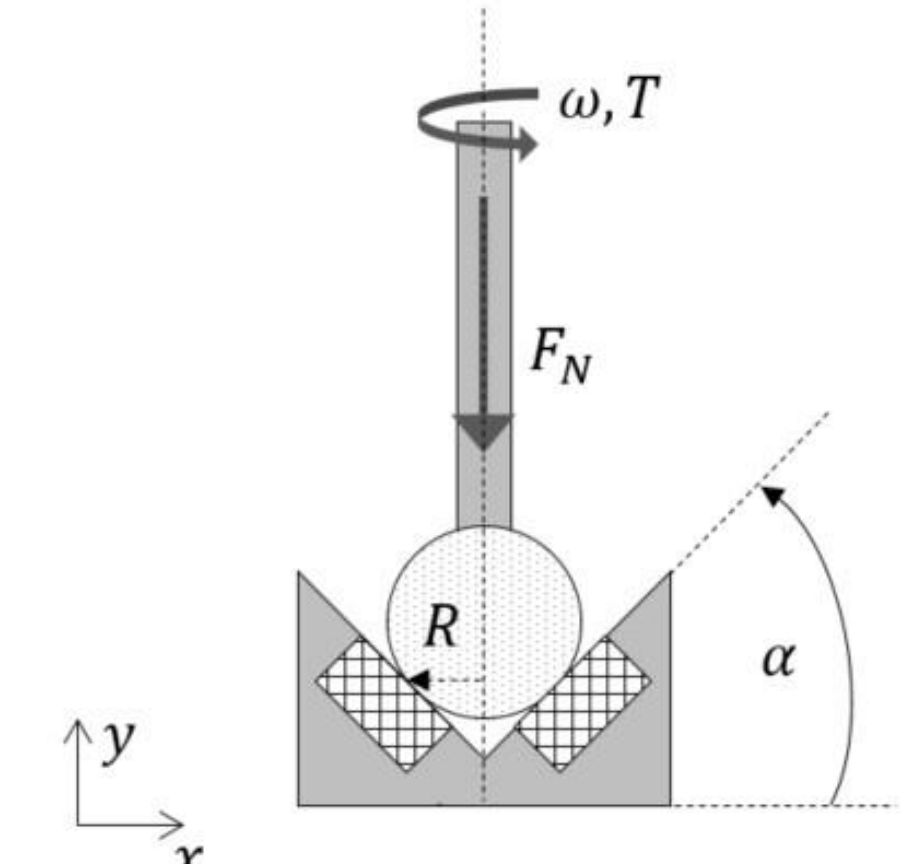


Fig. 4 Model tribosystem schematic

- Cocoa mass is a key component in many confectionery and chocolate products
- Wet grinding is a unit operation in cocoa mass processing
- Cocoa mass wet grinding yields particle size reduction

- Ground cocoa mass consists of particles which differ, e.g. in shape and size
- Wet grinding can also increase the free fat in the cocoa mass

- During food oral processing, the food material is mixed with saliva
- Tribological behavior of the tongue-bolus-palate tribosystem contributes to the mouthfeel
- The food structure and structural changes during food oral processing change the tribosystem behavior

- The real world tribosystem can be represented by tribological model systems with soft specimen
- Model system testing provides insights into the interrelationship between food structure and tribosystem behavior

## Cocoa mass: Structure, rheology and tribological testing

### Cocoa mass structure

- The same cocoa mass sample was used for every step of the characterization
- Sample was obtained by wet grinding on a horizontal disk mill
- Light microscopy pictures of the cocoa mass particles were taken on a Keyence VHX reflected light microscope equipped with a VH-Z500R objective (Keyence, Osaka Japan) after fat removal using acetone. An example picture can be seen in Fig. 2.
- The cocoa mass samples varied in particle size distribution. The volume equivalence diameter  $d_{90,3}$  from laser diffraction measurements based on the Fraunhofer scattering model carried out on a Mastersizer 3000 with wet dispersion unit (Malvern Panalytical, Malvern, United Kingdom) with synthetic mineral oil are shown in Fig. 6.

### Cocoa mass rheology

- Viscosity curve measurements were carried out at 40°C using a concentric cylinder measuring geometry on a Kinexus Prime ultra+ rotational rheometer (NETZSCH-Gerätebau GmbH, Selb, Germany).
- A logarithmic shear rate table from 1 s<sup>-1</sup> to 50 s<sup>-1</sup> was carried out after pre-shearing the sample at 5 s<sup>-1</sup> for 2 minutes.
- Shear viscosity data was fitted to the Herschel-Bulkley model  $\tau = \tau_0 + K\dot{\gamma}^n$  with the shear stress  $\tau$ , the yield stress  $\tau_0$ , the consistency index  $K$ , the shear rate  $\dot{\gamma}$  and the flow index  $n$ . The fitted parameters are shown in Table 1.

Table 1 Herschel-Bulkley fit parameters of tested cocoa mass samples

Sample	$\tau_0$ [Pa]	$K$ [Pa s <sup>n</sup> ]	$n$
Coarse $d_{90,3} = 33 \mu\text{m}$	2.55	2.36	0.951
Medium $d_{90,3} = 26 \mu\text{m}$	3.88	1.85	0.969
Fine $d_{90,3} = 20 \mu\text{m}$	3.30	1.55	0.960

### Tribological testing

- Testing at model scale was carried out at 40°C using a ball-on-three-pins tribology cell on a Kinexus Prime ultra+ rheometer and a Peltier-plate cartridge (NETZSCH-Gerätebau GmbH, Selb, Germany).
- The ball, 12.7 mm in diameter, was made of borosilicate glass.
- The pins were made of SIL 30 silicone urethane elastomer (Carbon Inc., Redwood City, USA) and were declined at 45°.
- Stribeck curves and extended Stribeck curve measurements (see also Pondicherry et al. 2018) were carried out with a minimum sliding speed of 2.25·10<sup>-8</sup> m·s<sup>-1</sup> and a maximum sliding speed of 4.5·10<sup>-1</sup> m·s<sup>-1</sup> and a constant normal force of 1 N after running-in at 15 rad·s<sup>-1</sup> during 10 min and a 5 min holding phase (see Fig. 5) (Rummel et al. 2023).

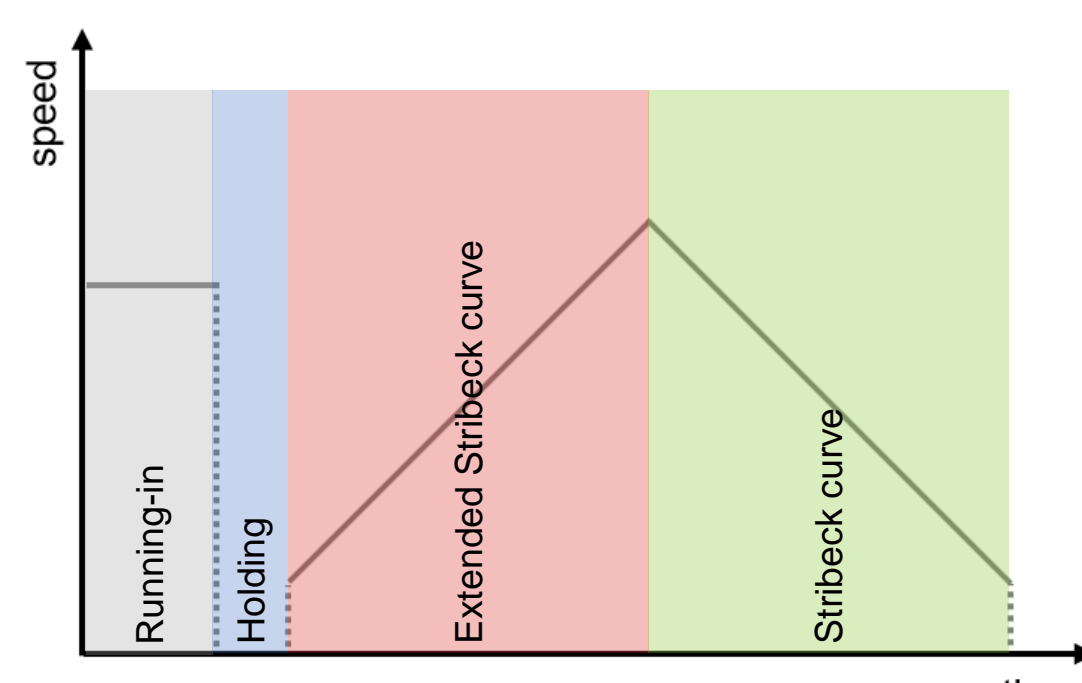


Fig. 5 Sequence of the tribological testing procedure

## Stribeck curves, extended Stribeck curves and discussion

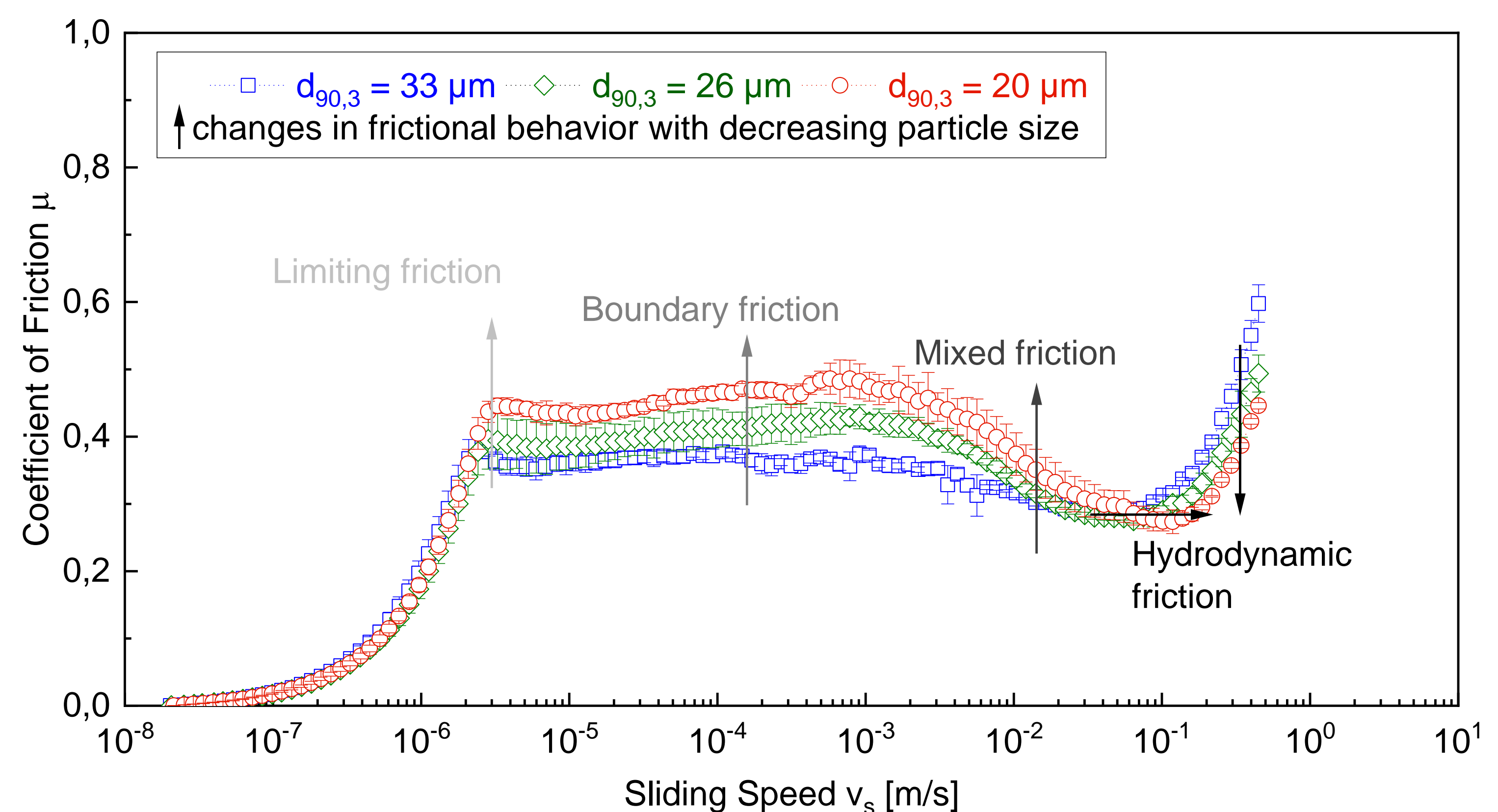


Fig. 6 Extended Stribeck curves for cocoa mass samples with different particle size distributions

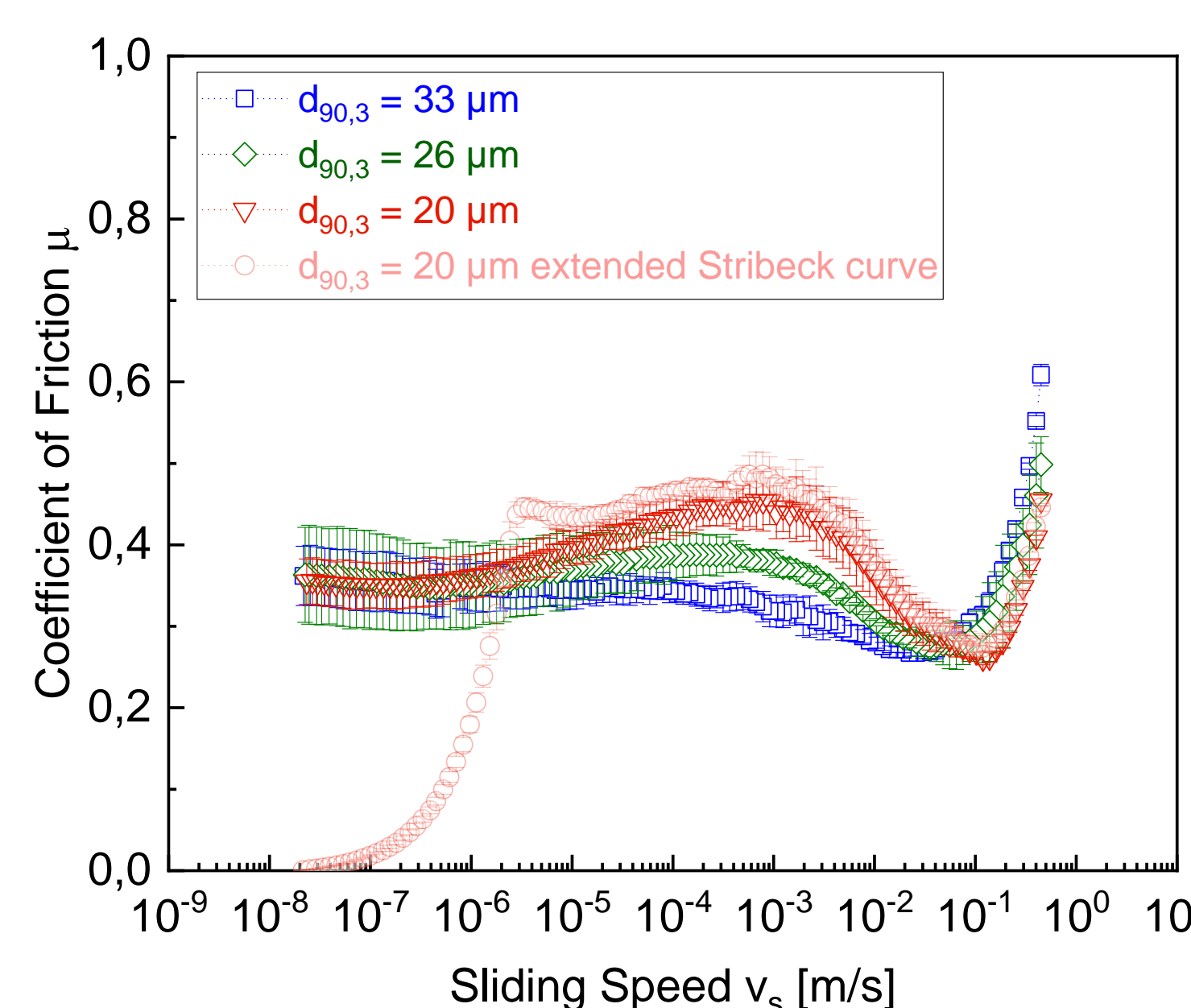


Fig. 7 Stribeck curves for cocoa mass samples with different particle size distributions

### Extended Stribeck curves

- Results from extended Stribeck curve measurements are shown in Fig. 6.
- The limiting friction is highest for the **fine cocoa mass sample**.
- After overcoming the limiting friction, the **fine cocoa mass sample** curve shows highest friction and the **coarse cocoa mass sample** exhibits the lowest friction.
- The friction in hydrodynamic regime is highest for **coarse cocoa mass sample** and lowest for the **fine cocoa mass sample**.

### Stribeck curves

- Results from Stribeck curve measurements are shown in Fig. 7.
- In the mixed friction regime and the hydrodynamic regime, the observed frictional behavior is similar to what was found in the extended Stribeck curve measurements.
- A local maximum in friction at intermediate speed (10<sup>-3</sup> m/s) can be seen for the **fine cocoa mass sample**.
- In the boundary friction regime, the curves for all three samples overlap.

### Possible lubrication mechanisms

Fig. 8 supports the understanding of the lubrications mechanisms explained in the following.

- Coarse particles acting as rollers (Rudge et al. 2020)
- Coarse particles too big to enter the tribocontact
- Non-spherical particles sterically hindered from entering the tribocontact
- Small particles sticking to the glass surface
- Small particles adhering to the soft elastomer surface (Lee et al. 2004)
- High numbers of particles causing increased interactions and interlocking. Small particles do not separate the specimen surfaces effectively (see also Rummel et al. 2023)

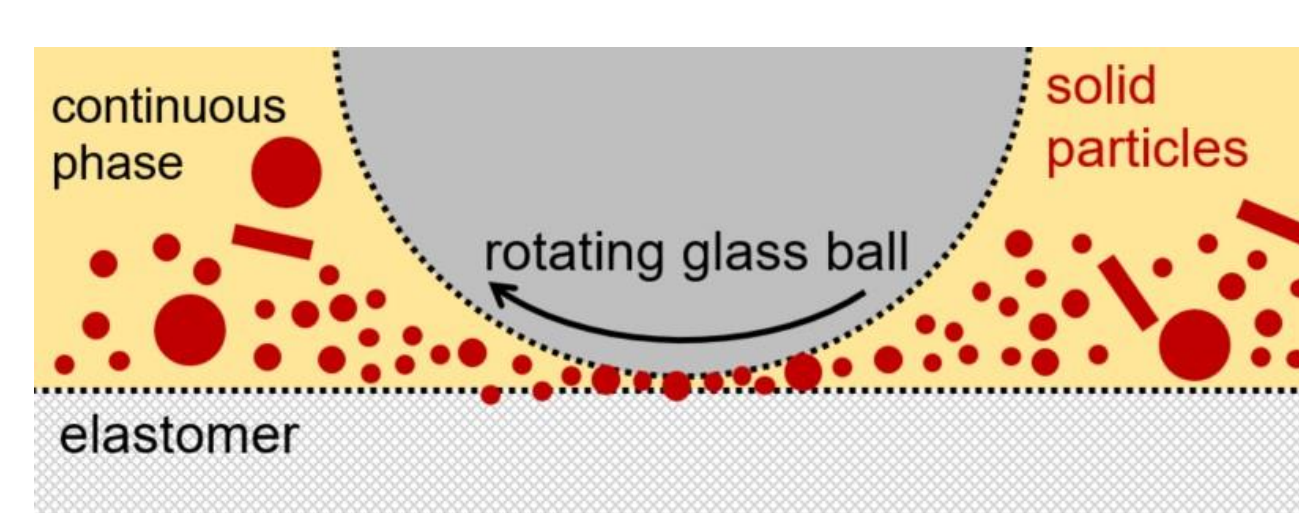


Fig. 8 Schematic of possible lubrication mechanisms

## References

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- Pondicherry K., Rummel F., Luger J., Extended Stribeck curves for food samples, Biosurface and Biotribology, 2018
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