

Consistency Between Methods: Thermal Conductivity Measurements of GPO-3 Fiberglass by GHFM, LFA and HFM

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Introduction

Polymer composites present a unique challenge in thermal conductivity measurements. With thermal conductivities often ranging from 0.2 to 1 W/(m·K), they can be challenging for common steady-state thermal measurement techniques such as the guarded hot plate (GHP) and heat flow meter (HFM) methods given their relatively high conductivities and rigid structure. Additionally, special precautions must be made to obtain accurate thermal properties using these techniques as they were designed for compressible insulations with thermal conductivities less than 0.1 W/(m·K). Laser or light flash analysis (LFA), on the other hand, was designed to measure homogeneous, isotropic materials and the inclusion of common fillers such as glass fibers may cause deviations in the temperature rise curve which must be accounted for using the proper model. This also necessitates the use of DSC (differential scanning calorimetry) to obtain specific heat capacity values to calculate thermal conductivity of such materials given the lack of comparable (anisotropic) reference standards in LFA. In contrast, the guarded heat flow meter (GHFM) technique was specifically designed to measure rigid materials with thermal conductivities ranging from 0.1 to 30 W/(m·K), making it a practical and straightforward method for evaluating the thermal properties of such materials.

To explore the viability of these techniques in the measurement of reinforced composites, GPO-3, an electrical-grade glass fiber reinforced thermoset with a polyester matrix, was measured using HFM, GHFM, LFA and DSC. GPO-3 is commonly used as an electrical insulator given its electrical and flame-retardant properties.

Experimental

Thermal conductivity was directly determined using both the TCT 716 *Lambda*® Guarded Heat Flow Meter and HFM 446 *Lambda*® by following the procedures laid out in their respective ASTM methods, ASTM E1530 and ASTM C518. Thermal diffusivity was determined using the LFA 467 *HyperFlash*® and specific heat capacity (c_p) was determined using the DSC 214 *Polyma*® by following ASTM E1461 and ASTM E1269, respectively. Thermal conductivity was then calculated using the measured values of specific heat capacity, thermal diffusivity and specimen density.

A single 305 by 305 mm plate of GPO-3 fiberglass with a thickness of approximately 6 mm was obtained from Polyply® Composites LLC for testing. The GPO-3 plate was first measured via HFM with the use of the instrumentation kit composed of silicone sheets and sample surface-mounted thermocouples which were used to reduce contact resistance between the specimen and instrument plates as well as to obtain accurate values of the sample surface temperature. The GPO-3 plate was measured at mean temperatures ranging from -10 to 80°C in 10°C increments. A temperature difference of approximately 6°C was held across the sample during testing. Calibration was performed using a borosilicate glass reference standard.

APPLICATIONNOTE Consistency Between Methods: Thermal Conductivity Measurements of GPO-3 Fiberglass by GHFM, LFA and HFM

Once the HFM measurements were complete, the board was then cut into four approximately 50 mm diameter discs for testing via GHFM (figure 1) and three approximately 12.5 mm diameter discs for testing via LFA. The four GHFM specimens were not modified in the through-thickness direction while the three LFA specimens were sanded down to a thickness of approximately 2 mm for testing.



1 GHFM test specimen (50 mm diameter), sectioned from a larger HFM board, with visible glass fiber reinforcement.

The GHFM measurements were conducted over a temperature range of approximately -10°C to 120°C in 10°C increments, and calibration was carried out using Vespel® SP-1. A thin layer of silicone thermal joint compound was applied between the specimens and instrument plates to minimize interfacial resistance. A pressure of approximately 175 kPa was applied to the specimens during testing. A temperature difference of roughly 24°C was held across the specimens during testing.

LFA measurements were similarly conducted over a temperature range of approximately -10°C to 120°C in 10°C increments. Specimens were spray coated with approximately 5 µm of graphite prior to testing. Thermal diffusivity was calculated using the NETZSCH Transparent [1] model which corrects for radiative effects seen in the temperature rise curve of the measurement. Specific heat capacity values determined via DSC were used in conjunction with the measured specimen density in order to obtain the thermal conductivity values.

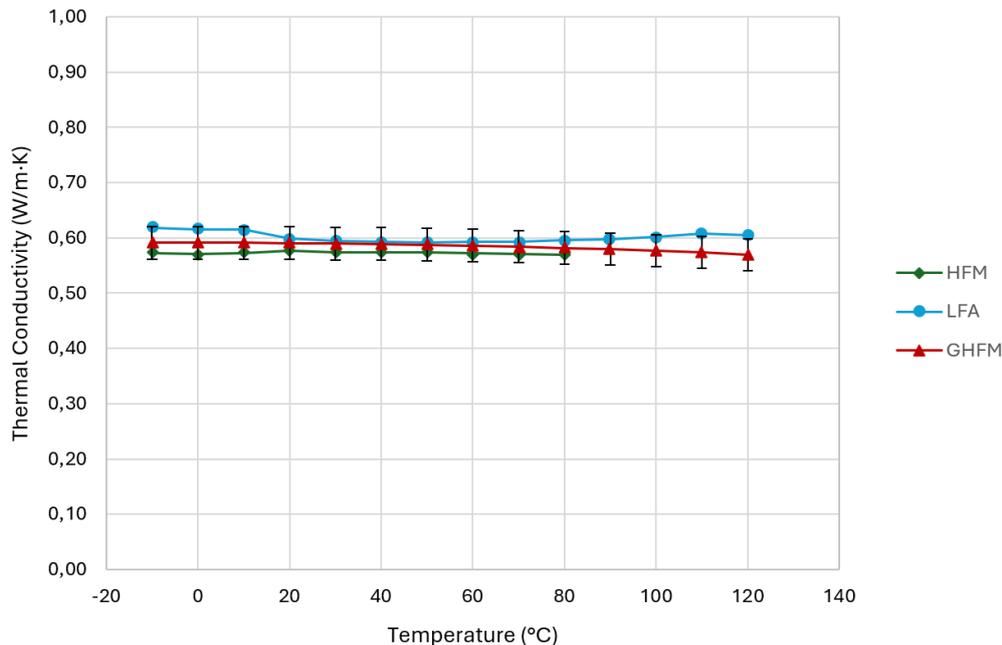
The 120°C maximum test temperature via GHFM and LFA was chosen to be safely below the mechanical U.L. Temperature Index value of 140°C to ensure the sample did not change from measurement to measurement and could withstand the 175 kPa the GHFM specimens were placed under [2].

Results and Analysis

It should be noted that the given results for all methods are not corrected for thermal expansion.

The thermal conductivity measurement results are illustrated in figure 2.

Thermal Conductivity vs. Temperature of GPO-3 Fiberglass



2 Thermal conductivity versus temperature of GPO-3 fiberglass as measured by three different methods: GHFM, HFM and LFA.

APPLICATIONNOTE Consistency Between Methods: Thermal Conductivity Measurements of GPO-3 Fiberglass by GHFM, LFA and HFM

Summary

Despite possible challenges in measuring fiber reinforced polymers, the results from each method showed consistency in the results. The error bars shown in Figure 1 are $\pm 5\%$ using the values measured via GHFM and nearly all obtained values of thermal conductivity from each method fall within this range. Thermal conductivity values reported for the GHFM were calculated based on a quadratic fit of the measured points generated by the measurement software. Thermal conductivity values reported for LFA were calculated from the material density, thermal diffusivity measured via LFA and specific heat capacity measured via DSC.

An increased measurement uncertainty must be expected for HFM and LFA results. The lower values of thermal conductivity obtained using HFM compared to the other two methods were anticipated due to the very low thermal resistance of the specimen, which was roughly $0.011 \text{ m}^2\cdot\text{K}/\text{W}$, nearly half of the limit of the technique as stated for the instrument of $0.02 \text{ m}^2\cdot\text{K}/\text{W}$. LFA results are not corrected for thermal expansion. Nevertheless, the results of this study indicate that it is possible to measure polymer matrix composites using a variety of techniques and obtain good agreement between methods.

References

1. Mehling, H, et al., "Thermal Diffusivity of Semitransparent Materials Determined by the Laser-Flash Method Applying a New Analytical Model", Int. J. Thermophysics, 19, 945, 1998.
2. PolyPly® Composites, Sheet Laminate Typical Properties, Accessed May 2025, Available: <https://www.polyplycomposites.com/sheet.pdf>